SERBIAN JOURNAL OF ELECTRICAL ENGINEERING Vol. 1, No. 3, November 2004, 1 - 6

Low-Frequency Plane Wave Diffraction On a Two-Layer Grating

Tatijana Dlabač ¹ , Dragan Filipović ²

Abstract: In this paper the problem of TE and TM plane wave diffraction from a two-layer grating in low-frequency case is presented. The problem is solved using the network model. Numerical results for the reflection coefficient of the lowest (n=0) mode versus frequency are given and compared to available results from literature.

Key words: Diffraction, Two-layer grating, Network model.

1 Introduction

Diffraction of a plane wave on single-layer and multi-layer gratings has been attracting scientists for a long time and it is still actually in present days. One of the most powerful tools for analysis of this problem is the Riemann-Hilbert method, which is presented in detail in monograph [1]. In the paper [2], the so-called network model for diffraction of a plane wave on a single-layer grating is presented, and in paper [3] simple analytical expressions for elements of that model are found. In this paper the network model is applied to the analysis of the diffraction of a plane wave on a two-layer grating in the low frequency case (grating period $\langle \times \lambda \rangle$). In that case network model is very simplified, because it does not take into account higher harmonics.

2 Network Model of the Problem

The geometry of the problem is shown on Fig. 1.

Fig. 1 *- Geometry of the problem.*

 1 Faculty of Maritime Studies, Dobrota 36, 85330 Kotor, Serbia&Montenegro

² Faculty of Electrical Engineering, Cetinjski put bb, 81000 Podgorica, Serbia&Montenegro

T. Dlaba~, D. Filipovi}

Gratings are identical, and their position is such that they would overlap when translated along the *z*-axis. Grating period is p , the distance between them is $-h$, and the distance between the strips is *a*. The medium is vacuum. Plane TM (or TE) polarized wave is incident perpendicularly on the gratings. The network model [2], which takes only the lowest ($n = 0$) mode into account, is the same in both cases and it is shown on Fig. 2.

The quantities on this figure are [3]:

$$
Y_{00} = j \frac{Y_0}{\frac{p}{\lambda} \ln \cos \frac{\pi a}{2p}}
$$
 (1)

for TE case and

$$
Y_{00} = -j4 \frac{p}{\lambda} Y_0 \ln \sin \frac{\pi a}{2p} \tag{2}
$$

for TM case, while $Y_0 = 1/120\pi$ is the wave admittance for vacuum.

Fig. 2 - *Equivalent network model.*

Reflection coefficient (for the lowest mode) can be obtained from Fig. 2,

$$
S_{11} = \frac{-\hat{Y}_{00} \left(2 + j\hat{Y}_{00} \text{ tg}\beta h\right)}{2 + 2j \text{ tg}\beta h + 2\hat{Y}_{00} + 2j\hat{Y}_{00} \text{ tg}\beta h + j\hat{Y}_{00}^{2} \text{ tg}\beta h},\tag{3}
$$

where

$$
\hat{Y}_{00} = \frac{Y_{00}}{Y_0} = 120\pi \cdot Y_{00}
$$
\n(4)

and

$$
\beta = \frac{2\pi}{\lambda} \,. \tag{5}
$$

Low Frequency Plan Waves Diffraction.....

3 Numerical Results

Diagrams of the reflection coefficient magnitude for the zero-mode in the TM case, for $h/\lambda = 0.5$ and for different values of a/p are shown on Figures 3-5 by solid lines. Calculations are made by using eqns. (2) , (3) , (4) and (5) .

Dashed lines on the same figures show reflection coefficient magnitude calculated by the approximate low-frequency formulas for the transmission coefficient [4]

Fig. 3 - *Reflection coefficient magnitude* for zero-mode in *TM case,* $a/p = 0.5$.

Diagrams of the reflection coefficient magnitude for the zero-mode in the TE case, for $h/\lambda = 0.5$ and for different values of a/p are shown of Figures 6-8 by solid lines. Calculations are made by using eqns. (1) , (3) , (4) and (5) .

Dashed lines on the same figures show reflection coefficient magnitude calculated by the approximate low-frequency formulas for the transmission coefficient [4]

$$
S_{21} = \frac{4\left(\frac{p}{\lambda}\right)^2 \ln^2 \cos \frac{\pi a}{2p} e^{j\beta h}}{4\left(\frac{p}{\lambda}\right)^2 \ln^2 \cos \frac{\pi a}{2p} + e^{2j\beta h}}.
$$
 (7)

T. Dlaba~, D. Filipovi}

Fig. 4 - *Reflection coefficient magnitude for zero-mode in TM case,* $a/p = 0.75$ *.*

Fig. 5 - *Reflection coefficient magnitude for zero-mode in TM case,* $a/p = 0.9$ *.*

Low Frequency Plan Waves Diffraction.....

Fig. 6 - *Reflection coefficient magnitude for zero-mode in TE case,* $a/p = 0.25$ *.*

Fig. 7 - *Reflection coefficient magnitude for zero-mode in TE case,* $a/p = 0.5$ *.*

As one can see from Figures 3-8, in the low-frequency case ($p/\lambda \ll 1$), when higher harmonics can be neglected, our results based on the network model are in agreement with available results from the literature.

T. Dlaba~, D. Filipovi}

Fig. 8 - *Reflection coefficient magnitude for zero-mode in TE case,* $a/p = 0.75$ *.*

4 Conclusion

In this paper diffraction problem of TE and TM polarized plane wave on a two-layer grating for perpendicular incidence and the low-frequency case ($p \ll \lambda$) is discussed. The problem is solved using network model, which does not take into account higher harmonics. Reflection coefficient magnitude is calculated and shown versus the relative period p/λ .

The obtained results are in good agreement with the available results from the literature.

References

- [1] В. П. Шестопалов: Метод задачи Римана Гилберта в теории дифракции и распространения злектромагнитных волн, Харьков, 1971.
- [2] M. Guglielmi, A. A. Oliner: Multimode network description of a planar periodic metal-strip grating at a dielectric interface - Part I, IEEE Trans. Microwave Theory Tech., Vol. 37, pp. 534-541, March 1989.
- [3] D. Filipović: New explicit expressions for the coupling matrix elements related to scattering from a planar periodic single' strip grating, IEEE Trans. Microwave Theory Tech., Vol. 43, pp. 1540-1544, 1995.
- [4] В. П. Шестопалов, A. A. Kириленко, С. А. Масалов, Ю. К. Сиренко: Резонансное рассеянние волн - T1: Дифракционные решетки, Киев, 1986.